

NGL C12 Pore Volume Calculation

Lyons

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.65	82.5	2.47	0.1073	8.8500
				$\Sigma(\phi * h) =$	8.8500

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = 8,627,625 \text{ bbl}$$

Total Volume

$$V = 40,073,050 \text{ bbl}$$

Net Pay

$$h = 309 \text{ ft}$$

L Satanka

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.65	0	2.65	0.0000	0.0000
				$\Sigma(\phi * h) =$	0.0000

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = - \text{ bbl}$$

Average ϕ

$$\phi = 0.133$$

Wolfcamp

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.87	0	2.87	0.0000	0.0000
				$\Sigma(\phi * h) =$	0.0000

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = - \text{ bbl}$$

Amazon

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.87	31.5	2.38	0.2636	8.3045
				$\Sigma(\phi * h) =$	8.3045

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = 8,095,876 \text{ bbl}$$

Council Grove

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.87	86.8	2.65	0.1187	10.3046
				$\Sigma(\phi * h) =$	10.3046

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = 10,045,674 \text{ bbl}$$

Admire

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.87	4	2.72	0.0791	0.3166
				$\Sigma(\phi * h) =$	0.3166

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = 308,623 \text{ bbl}$$

Virgil

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.87	12	2.60	0.1444	1.7326
1.00	2.71	9.8	2.61	0.0585	0.5731
				$\Sigma(\phi * h) =$	2.3057

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = 2,247,784 \text{ bbl}$$

Fountain

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.87	63	2.59	0.1481	9.3321
1.00	2.71	8	2.51	0.1199	0.9591
				$\Sigma(\phi * h) =$	10.2911

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = 10,032,563 \text{ bbl}$$

Missouri

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.65	11	2.54	0.0667	0.7333
				$\Sigma(\phi * h) =$	0.7333

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = 714,907 \text{ bbl}$$

Desmoines

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.65	0	2.65	0.0000	0.0000
				$\Sigma(\phi * h) =$	0.0000

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = - \text{ bbl}$$

Atoka

ρ_{fr} , gm/cc	ρ_{ma} , gm/cc	h, ft	ρ_{br} , gm/cc	ϕ	$\phi * h$, ft
1.00	2.65	0	2.65	0.0000	0.0000
				$\Sigma(\phi * h) =$	0.0000

Volume Calculation

$$B_w = 1.00$$

$$S_w = 1.00$$

$$r = 1320 \text{ ft}$$

$$V = - \text{ bbl}$$