

Whiting Oil & Gas Corp.
Razor 26L-3503A Sidetrack Drill Plan
June 18, 2014

Summary:

The Razor_26L-3503A well will be a horizontal well in the Niobrara formation. The well will be drilled to the sidetrack KOP at 5,597' TVD. A curve will be built to land the 7" casing in the Niobrara at 5,605' TVD. The lateral will be drilled with a 6" bit to TD at 12,480' MD. 4-1/2" casing with swell packers will be run in the lateral for completion.

Surface Location: 26-T10N-R58W
2319' FSL 660' FWL
Weld County, Colorado

Bottomhole Location: 35-T10N-R58W
600' FSL 825' FWL
Weld County, Colorado

DRILLING PROGRAM

1. ESTIMATED TOPS OF GEOLOGICAL MARKERS:

Ground Level 4,735' Estimated KB 4,751' (16.5')

<u>Formation</u>	<u>MD</u>	<u>Lithology</u>	<u>Hazard</u>
Fox Hills	Surface	Sandstone, shale, coal	Water
Pierre	1,406'	Ss and dark grey shale	None
Niobrara	5,484'	Chalk, limey shale, shale	Oil, gas, fractures
Horizontal Target (TVD)	5,587'	Chalk, marl	Oil, gas, fractures
TD Niobrara Horizontal (MD)	12,480'		

2. DIRECTIONAL PLANS

KOP: 5,076' MD, 5,597' TVD
BUILD RATE - AZIMUTH: 11°/100', 165.20° Azimuth
END OF BUILD: 6,006' MD, 5,600' TVD at 82.68° Inc and 179.15° Azimuth
7" CASING POINT: 6,006' MD, 5,600' TVD at 82.68° Inc and 179.15° Azimuth
7" CSG POINT COORDINATES: 1778' FSL & 1044' FWL Sec 26 T10N R58W
Sidetrack KOP: 7,000' MD, 5,597' TVD
TD LATERAL: 12,480' MD, 5,605' TVD at 90.00° Inc and 181.07° Azimuth
BH LOCATION: 600' FSL & 825' FWL Sec 35 T10N R58W

See attached Directional Proposal Listings for more details.

3. PRESSURE CONTROL EQUIPMENT

A. Type: Eleven (11) inch double gate hydraulic BOP with eleven (11) inch annular preventer with 5,000 psi Casinghead and 5,000 psi Tubinghead.

B. Testing Procedure:

The annular preventer will be pressure tested to 50% of stack rated working pressure for ten (10) minutes or until provisions of test are met, whichever is longer. The BOP, choke manifold, and related equipment will be pressure tested to approved BOP stack working pressure (if isolated from surface casing by a test plug) or to 70% of surface casing internal yield strength (if BOP is not isolated by a test plug). Pressure will be maintained for ten (10) minutes or until the requirements of the test are met, whichever is longer. At a minimum, the Annular and Blow-Out Preventer pressure tests will be performed:

1. When the BOPE is initially installed;
2. Whenever any seal subject to test pressure is broken;
3. Following related repairs; and
4. At thirty (30) day intervals.

Annular will be function tested weekly, and pipe & blind rams activated each trip, but not more than once per day. All BOP drills & tests will be recorded in IADC driller's log.

C. Choke Manifold Equipment:

All choke lines will be straight lines whenever possible at turns, tee blocks will be used or will be targeted with running tees, and will be anchored to prevent whip and vibration.

D. Accumulator:

Accumulator will have sufficient capacity to open hydraulically-controlled choke line valve (if so equipped), close all rams plus annular preventer, and retain a minimum of 200 psi above precharge on the closing manifold without the use of closing unit pumps. The fluid reservoir capacity will be double accumulator capacity and the fluid level will be maintained at manufacturer's recommendations. Accumulator precharge pressure test will be conducted prior to connecting the closing unit to the BOP stack.

E. Miscellaneous Information:

Choke manifold and BOP extension rods with hand wheels will be located outside rig sub-structure. Hydraulic BOP closing unit will be located at least twenty-five (25) feet from the wellhead but readily accessible to the driller. Exact locations and configurations of the hydraulic BOP closing unit will depend upon the particular rig contracted to drill this hole.

A flare line will be installed after the choke manifold with the discharge point of the flare line to a separate pit located at least 125 feet away from the wellbore and any existing production facilities.

A volume monitoring system with alarms will be used to monitor pit gains/losses along with visual backup.

4. PROPOSED CASING PROGRAM

A. Casing Program: All New

Hole Size	Casing Size	Wt./Ft.	Grade	Joint	Coupling OD	Burst (psi)	Collapse (psi)	Tension (Body/Joint) (klbs)	Depth Set (md)
13-1/2"	9-5/8"	36	J-55	LT&C	10.625"	3,520	2,020	564/453	0 – 1,528'
8-3/4"	7"	29	L-80	LT&C	7.656"	8,160	7,020	676/587	0 – 6,006'
6"	4-1/2"	11.6	L-80	LT&C	5"	7,780	6,350	267/212	6,006' – 12,480'

9-5/8" surface casing will have centralizers as follows:

1. Install a bowspring centralizer at the first and second collars above the guide shoe.
2. Install one bowspring centralizer every third joint above the second collar.
3. Centralizer and basket placed 120' below the surface (or at the bottom of the third joint below the surface).
4. Centralizer and basket placed 80' below the surface (or at the bottom of the second joint below the surface).

7" production casing will have centralizers as follows:

1. Install floating standoff bands (positive standoff centralizers) one each joint to KOP.
2. After that centralize every third joint to surface with single bow spring centralizers.

4-1/2" Liner to be run with Swelling Packers and Frac Sleeves

Casing string(s) will be pressure tested to 0.22 psi/foot of casing string length or 1500 psi, whichever is greater (not to exceed 70% of the internal yield strength of the casing), after cementing and prior to drilling out from under the casing shoe.

B. Casing Design Parameters: Surface Casing (Existing)

Interval	Size	Wt	Grade	Burst (psi) ^a /SF	Collapse (psi) ^b /SF	Tension (klb) ^c /SF
0' – 1,528'	9-5/8"	36.0 lb/ft	J-55	3,520/3.33	2,020/2.88	453/9.73

- a. based on frac gradient at shoe of 14.0 ppg
- b. based on full evacuation with 9.0 ppg fluid on backside
- c. based on casing string weight in 9.0 ppg mud
String Weight in 9.0 ppg mud ≈ 46,580 lbs

Production Casing (Existing)

Interval	Size	Wt	Grade	Burst (psi) ^a /SF	Collapse (psi) ^b /SF	Tension (klb) ^c /SF
0' – 6,006'	7"	29.0 lb/ft	L-80	8,160/1.26	7,020/2.20	587/4.05

- a. based on 6,500 psi frac pressure.
- b. based on full evacuation with 11 ppg pore pressure on backside
- c. based on casing string weight in 10.0 ppg mud
String Weight in 10.0 ppg mud ≈ 144,828 lbs.

Production Liner

Interval	Size	Wt	Grade	Burst (psi) ^a /SF	Collapse (psi) ^b /SF	Tension (klb) ^c /SF
6,006'–12,480'	4-1/2"	11.6 lb/ft	L-80	7,780/1.44	6,350/1.75	212/3.00

- a. based on 6,500 psi frac pressure.
- b. based on full evacuation with 12.5 ppg pore pressure on backside
- c. based on casing string weight in 10.0 ppg mud
String Weight in 10.0 ppg mud ≈ 70,653 lbs.

5. PROPOSED CEMENTING PROGRAM

Surface Casing

CASING	SLURRY	FT. of FILL	CEMENT TYPE	SXS	XC (%)	WEIGHT (ppg)	YIELD (ft ³ /sx)
9-5/8"	Lead	1,528'	Type III Cement + 0.08 lbs/sack Static Free + 1% bwoc Calcium Chloride + 0.25 lbs/sack Cello Flake + 60.4% Fresh Water.	719	35	14.5	1.40

A cement top job is required if cement fallback is greater than 10' below ground level.

Production Casing

CASING	SLURRY	FT. of FILL	CEMENT TYPE	SXS	XC (%)	WEIGHT (ppg)	YIELD (ft ³ /sx)
7"	Lead	4,500'	(35:65) Poz (Fly Ash):Class G Cement + 0.06 lbs/sack Static Free + 0.1% bwoc R-3 + 46.46% bwoc LW-6 + 1% bwoc FL-25 + 0.5% bwoc Sodium Metasilicate + 5% bwoc CSE-2 + 85% Fresh Water.	317	30	10.5	2.64
7"	Tail	1,394'	315 cu-ft; 101 sacks (35:65) Poz (Fly Ash):Class G Cement + 0.06 lbs/sack Static Free + 54.44% bwoc LW-6 + 1% bwoc FL-25 + 0.5% bwoc Sodium Metasilicate + 20% bwoc Silica Sand, 100 mesh, Sacked + 5% bwoc CSE-2 + 100.6% Fresh Water.	96	35	10.5	3.12

Cement volumes for the 7" Production Casing will be calculated to provide a top of cement to Surface.

All waiting on cement (WOC) times will be adequate to achieve a minimum of 500 psi compressive strength at the casing shoe prior to drilling out.

Production Liner

CASING	SLURRY	FT. of FILL	SXS	XC (%)	CEMENT TYPE	WEIGHT (ppg)	YIELD (ft ³ /sx)
4-1/2"	Tail	7188	495	15	495 sx (50:50) POZ (Fly Ash): Class G Cement +0.27% BWOC FL-63 +0.6% BWOC +FL-52+3% BWOC Bentonite+ 20% BWOC Silica + Flour+0.2% BWOC BA-59 +61.5% Fresh Water	14.5	1.44

6. MUD PROGRAM

<u>Depth (MD)</u>	<u>Mud System</u>	<u>MW</u>	<u>PV</u>	<u>YP</u>	<u>FL</u>
0 -1,528'	Water, Gel/Lime Sweeps	8.4 – 8.5	0 - 6	0 - 4	NC
1,528' – 6,006'	Water, Gel/Lime Sweeps	8.4 – 8.5	0 - 6	0 - 4	NC
6,006' – 12,480'	LSND	8.7 – 9.2	8 - 20	8 - 14	10 - 12

7. EVALUATION PROGRAM

Cores: None planned

DST: None planned

Surveys: Deviation surveys every 500' to TD in both surface and production holes.

Mud Logger:

Samples: 30' samples surface to 5,540'
10' samples 5,540' to TD

Open Hole Logging Program: None planned

8. ABNORMAL CONDITIONS

No abnormal pressures are anticipated. No H₂S gas is anticipated.

Anticipated bottom hole pressure is 2,419 psi (0.433 psi/ft) at 5,587' TVD in the Niobrara and the maximum anticipated surface pressure equals approximately 1,190 psi (anticipated bottom hole pressure minus the pressure of a partially evacuated hole calculated at 0.22 psi/foot of hole).

9. ANTICIPATED STARTING DATES

A. Anticipated Starting Dates:

Dirt work startup: June 2013

Spud: June 2013

Duration: 25 – 35 days