

Peakview Operating Company, LLC
Grassy Creek 13-26
 SHL: 2,009' FSL 998' FWL (NW/4 SW/4)
 BHL: ±1,947' FSL ±717' FWL (NW/4 SW/4)
 Sec. 26 T6N R87W, 6th P.M.
 Routt County, Colorado
 Surface: Fee
 Mineral Lease: Fee

DRILLING PROGRAM

(All Drilling Procedures will be followed as Per Onshore Orders No. 1 and No. 2)

Please contact Kim Rodell at 303-942-0506, if there are any questions or concerns regarding this Drilling Program.

SURFACE ELEVATION – 7,077' (Un-graded ground elevation)

SURFACE FORMATION – Almond – Freshwater possible

ESTIMATED FORMATION TOPS

Formation	True Vertical Depth	Measured Depth	Geology
Williams Fork	Surface	Surface	Sandstone, Siltstone, Shale & Minor Coal
BWF	300'	300'	Sandstone, Shale & Coal
Trout Creek	650'	650'	Sandstone
Iles	1,800'	1,800'	Sandstone, Shale & Coal
Mancos	2,088'	2,088'	Sandstone, Shale & Coal
Fresh Water	2,258'	2,258'	Sandstone, Shale & Coal
Maraposa	3,005'	3,005'	Sandstone, Shale
Niobrara	5,430'	5,455'	Sandstone, Shale
Buck Peak Bench	5,430'	5,455'	Sandstone, Shale & Limestone
Tow Creek	5,804'	5,829'	Sandstone, Shale & Limestone
Wolf Mountain	6,019'	6,044'	Sandstone, Shale & Limestone
Codell	6,535'	6,560'	Sandstone, Shale & Limestone
Total Depth	6,735'	6,760'	

ESTIMATED DEPTHS OF ANTICIPATED WATER, OIL, GAS, OR MINERAL BEARING FORMATIONS

Estimated depths at which water, oil, gas or other mineral-bearing formations are expected to be encountered:

Formation	True Vertical Depth(TVD)	Measured Depth(MD)	Lithology
Almond	Surface	Surface	Some Water, Oil & Gas Bearing
BWF	300'	300'	Some Water, Oil & Gas Bearing
Trout Creek	650'	650'	Some Water, Oil & Gas Bearing
Iles	1,800'	1,800'	Some Water, Oil & Gas Bearing
Mancos	2,088'	2,088'	Some Water, Oil & Gas Bearing
Fresh Water	2,258'	2,258'	Some Water, Oil & Gas Bearing
Maraposa	3,005'	3,005'	Some Water, Oil & Gas Bearing
Niobrara	5,430'	5,455'	Some Oil & Gas Bearing

Buck Peak	5,430'	5,455'	Some oil & gas bearing
Tow Creek	5,804'	5,829'	Some oil & gas bearing
Wolf Mountain	6,019'	6,044'	Some oil & gas bearing
Codell	6,535'	6,560'	Some oil & gas bearing
Total Depth	6760' MD		
	6735' TVD		

All fresh water and prospectively valuable minerals encountered during drilling will be recorded by depth and protected.

CASING PROGRAM

Total Depth (MD)	Hole Diameter	Casing Diameter	Casing Weight and Grade	Cement
0 – 120'	26"	20"	Conductor- 20",94#/ft,H40, ST&C- Casing	Cement to surface (±315 sxs Halcem V1 – Class G base) *
0' – 2658'	14-3/4"	9-5/8"	36#/ft, J-55 LT&C Casing	Cement to surface, DV tool at 1500' MD(1 stage –shoe – lead 400 sxs Varicem V1 , tail - 410 sxs Varicem V1, stage 2 thru DV tool – Lead - 845 sxs Varcem V1 cmt. Tail - 100 sxs Varicem V1) *
2658' – 5455'	8-3/4"	7"	23#/ft, N-80 LT&C Casing	TOC at 1600'MD (1000' overlap inside surface csg) DV Tool set at 3000'MD,1 stage thru shoe - Lead 145 sxs Econocem V4 cmt, Tail 170 sxs Expandacem V3 cmt., 2 nd stage thru DV tool - Lead 80 sxs Econocem V4 cmt. Tail 50 sxs Halcem cmt. **
5455' – 6760'	6-1/8"	4-1/2"	10.5 #/ft, K-55, LT&C Pre-perforated Liner	No cement – Open Hole completed w/ Slotted liner to TD and Top of Liner landed at 5255'MD

* Cement volume calculated with 100% excess.

** Cement volume calculated with 60% excess.

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	Conductor:		Halcem V1 class G base cmt.	Yield: 1.17 ft ³ /sx, Weight: 15.8ppg Water: 5.02 Gal/sk
	Surface:	Stage 1 Lead & Tail	Varicem V1 Cement	1 stg –Lead: Yield 2.24 ft ³ /sk, Weight: 12.3 ppg, Tail: Yield 1.72 ft ³ /sk, Weight: 13.5 ppg.
	Surface:	Stage 2: Lead & Tail:	Varicem V1 Cement	Lead 2 nd stg: Yield 2.24 ft ³ /sx, Weight: 12.3 ppg, Tail Yield 1.72 ft ³ /sk, Weight 13.5 ppg
	Intermediate	Stage 1: Lead Tail	Econocem V4 Expandacem V3	Lead-1 st stg: Yield 2.48 ft ³ /sk, Weight: 11.5 ppg Tail – 1 st stg: Yield 1.50 ft ³ /sk, Weight: 13.5 ppg
		Stage 2: Lead: Tail	Econocem V4 Halcem	Lead-2 nd stg: Yield 2.45 ft ³ /sk, Weight 11.5 ppg Tail Yield 1.15 ft ³ /sk, weight 15.8 ppg

Surface casing top job will be 100' will use 1" tubing, with Class "G" cement with 2% CaCl₂ if necessary.

Cement additives – (Note: Some additives are Halliburton proprietary products. If another cement contractor is used, these blends and products may vary slightly).

Cement additives:

Conductor:			Halcem V1 – Class G base cement
Surface:	Stage 1	Lead	Varicem V1 cmt, .125 lbm/sk Poly Flake, 0.2% Fe-2, Type III base cement
Surface	Stage 1	Tail	Varicem V1 cmt., .125 lbm/sk Poly-flake, Type III base cement
Surface	Stage 2	Lead	Varicem V1 cmt, .125 lbm/sk Poly Flake, type III base cement
Surface	Stage 2	Tail	Varicem V1 cmt, .125 lbm/sk Poly flake, Type III base cement
Intermediate	Stage 1	Lead	Econocem V4 cmt., 3 lbm/sk Kol-seal, 0.2 % HR-800, Type V Cement and Poz base system
Intermediate	Stage 1	Tail	Expandacem V3 cmt., 0.4 % HR-800, 1lbm/sk Poly-flake, Class G and Poz base system
Intermediate	Stage 2	Lead	Econocem V4 cmt., Type V Cement and Poz base system
Intermediate	Stage 2	Tail	Halcem cmt., 0.1 % HR-5, Class G base cement

PRESSURE CONTROL

- See attached blowout preventer diagram.

BOPs and choke manifold will be installed and pressure tested before drilling out of surface casing (subsequent pressure test will be performed whenever pressure seals are broken), and then will be checked daily as to mechanical operating condition. BOPs will be pressure tested at least once every 30 days. Ram type preventers and related pressure control equipment will be pressure tested to related working pressure of the stack assembly if a test plug is used. If a plug is not used, the stack assembly will be tested to the rated working pressure of the stack assembly or 70% of the minimum internal yield of the casing, whichever is less. Annular type preventers will be pressure tested to 50% of their working pressure. All casing strings will be pressure tested to 0.22 psi/ft or 1,500 psi, whichever is greater, not to exceed 70% of the internal yield. If a 5M system or greater is used, the casing shoe will be tested by drilling 5-20' out from under the shoe and pressure tested to a maximum expected mud weight equivalent as shown in the mud program listed below.

A manual locking device (i.e. hand wheels) or automatic locking devices shall be installed on the BOP stack. Remote controls capable of both opening and closing all preventers shall be readily accessible to the driller.

The choke manifold and accumulator will meet or exceed Onshore Order No. 2 (OSO #2) standards. The BOP equipment will be tested after any repairs to the equipment. Pipe rams, blind rams and annular preventer will be activated on each trip and weekly BOP drills will be conducted with each crew. All tests, maintenance, and BOP drills will be documented on rig "tower sheets".

Statement of Accumulator System and Location of Hydraulic Controls

The drilling rig has not been selected for this well. Selection will take place after approval of this application is granted. Manual and/or hydraulic controls will be in compliance with OSO #2 for 2,000 psi system.

A remote accumulator will be used. Pressures, capacities, location of remote hydraulic and manual controls will be identified at the time of the COGCC supervised BOP test.

MUD PROGRAM

0' - 120' MD	Fresh Water M.W.: 8.4 Visc.: 40 FL N/A
120' - 2,658' MD	Spud Mud M.W.: 8.4 – 8.6 ppg Visc.: 28 – 30 WL: N/C pH: 7.5 – 8.5 Yield: 4 – 8 LGS: ≤ 4%
2,658' MD - 5455' MD	DAP Fluid (Dimonium Phosphate) M.W.: 8.6 – 9.4 ppg Visc.: 28 – 35 WL: ≥ 10 pH: 7.5 – 8.3 Yield: 10 – 16 LGS: ≤ 4%
5455' MD - 6760' MD	Amodrill 1410 - Synthetic Olefin Fluid M.W.: 6.1 – 7.5 ppg, Density .733 relative to water of 1.0 mg/l Visc.: 10 – 30 WL: N/A Yield: 10 – 12 LGS: ≤ 2 %

Sufficient mud materials to maintain mud properties, control lost circulation and to contain a “kick” will be available on location.

AUXILIARY EQUIPMENT

- A. Upper Kelly cock; lower Kelly cock will be installed while drilling and tested with 5000 psi BOP.
- B. Inside BOP or stabbing valve with handle (available on rig floor).
- C. Safety valve(s) and subs to fit all string connections in use.
- D. Mud monitoring will be with a flow sensor, pit level indicator, and visual observation.

LOGGING, CORING TESTING PROGRAM

- A. Logging: CBL will be run on surface and intermediate.
Open-hole logging from TD – 5,000'
Platform Express, Array Induction, Lithio density/ Compensated Neutron,
Bi-pole Sonic, FMI.
- B. Coring: None planned – Whole core or rotary sidewall cores as warranted.
- C. Testing: None planned – Drill Stem tests may be run on shows of interest.

ABNORMAL CONDITIONS

- A. Pressures: No abnormal conditions are anticipated.
Anticipated maximum BHP gradient: 0.45 psi/ft
True bottom-hole anticipated pressure $\pm 2,100$ psi taken from completed offset producers.
- B. Temperatures: No abnormal conditions are anticipated.
- C. H₂S: None Anticipated.
- D. Estimated bottom-hole pressure: 3,031 psi

ANTICIPATED START DATE

June 1, 2013

COMPLETION

The location pad will be sufficient size to accommodate all completion equipment activities and equipment. A string of 2-7/8" 6.5#, N-80, 8rnd EUE will be run as production tubing. A Sundry Notice (SN) will be submitted with a revised completion program if warranted.

Well Name: Grassy Creek 13-26
 Location: NW SW, Sec 26, T6N, R87W, 6th P.M.
 SHL: 2008.8' FSL & 998.2' FWL
 BHL: 1947.1' FSL & 717.0' FWL
 County: Routt
 State: Colorado

Operator: Peakview Operating Company LLC.

SURFACE CASING

Size	Weight	Grade	Conn	
9-5/8"	36.00	J-55	LT&C	
Setting Depth of Surface Casing:				2,658'
TD of Next Hole Section:				5,455'
Press Gradient @ This Depth:				0.45 psi/ft
Press Gradient of Formation Fluid:				0.22 psi/ft
BHP @ 5,455'				2,455 psi
Hydrostatic Head of Form Fluid @ 5,455'				1,200 psi
Max Design Surface Pressure:				1,255 psi

Casing Specs For: 9-5/8", 36.00 ppf, J-55, LT&C

100% STRENGTHS

COLLAPSE	BURST	TENSION
2,020	3,520	453,000

DESIGN SAFETY FACTORS

COLLAPSE:	1.125
BURST:	1.0
TENSION:	1.8

CALCULATED SAFETY FACTORS

COLLAPSE:	1.7	OK
BURST:	2.8	OK
TENSION:	4.7	OK

CALCULATED SAFETY FACTORS

Collapse:
 Hydrostatic Pressure: 0.052 8.7 ppg 2,658' = 0.052 X 8.7 X 2,658' = 1202 psi
 Safety Factor (Collapse): 2,020 psi 1,202 psi 1.7 OK

Safety Factor (Burst): 3,520 psi 1,255 psi 2.8 OK

Tension:
 Safety Factor (Tension): 36.00 ppf 2,658' = 36 X 2,658' = 95,688 lbs
 453,000 95,688 = 453,000 / 95,688' = 4.7 OK

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INTERMEDIATE CASING

Size	Weight	Grade	Conn
7"	23.00	N-80	LT&C

Setting Depth of Intermediate Casing: 5,455'
 TD Of Next Hole Section: 6,760' MW Behind Surface: 8.7 ppg @ 5,455'
 Press Gradient @ This Depth: 0.44 psi/ft MW At Next Section TD: 9.5 ppg @ 6,760'
 Press Gradient of Formation Fluid: 0.22 psi/ft
 BHP @ 6,760' 2,974 psi
 Hydrostatic Head of Form Fluid @ 6,760' 1,487 psi
 Max Design Surface Pressure: 1,487 psi

Casing Specs For: 7", 23.00 ppg, N-80, LT&C

100% STRENGTHS

COLLAPSE	BURST	TENSION
3,830	6,340	442,000

DESIGN SAFETY FACTORS

COLLAPSE:	1.125
BURST:	1.0
TENSION:	1.8

CALCULATED SAFETY FACTORS

COLLAPSE:	1.6	OK
BURST:	4.3	OK
TENSION:	3.5	OK

CALCULATED SAFETY FACTORS

Collapse:
 Hydrostatic Pressure: 0.052 8.7 ppg 5,455' = 0.052 X 8.7 X 5,455' = 2468 psi
 Safety Factor (Collapse): 3,830 psi 2,468 psi 1.6 OK
 Safety Factor (Burst): 6,340 psi 1,487 psi 4.3 OK
 Tension: 23.00 ppg 5,455' = 23 X 5,455' = 125,465 lbs
 Safety Factor (Tension): 442,000 125,465 = 442,000 / 125,465' = 3.5 OK

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 State: Colorado

Operator: Peakview Operating Company LLC.

PRODUCTION CASING

Size	Weight	Grade	Conn
4-1/2"	10.50	N80	ST&C
Setting Depth of Production Casing:			6,760'
Hole Total Depth:			6,760'
Press Gradient @ This Depth:			0.433 psi/ft
Press Gradient of Formation Fluid:			0.22 psi/ft
BHP @ 6,760'			2,927 psi
Hydrostatic Head of Form Fluid @ 6,760'			1,487 psi

MW Behind Production Casing: 9.5 ppg @ 6,760'
 MW At TD: 9.5 ppg @ 6,760'

Max Design Surface Pressure: 1,440 psi

Casing Specs For: 4-1/2", 10.50 ppf, N80, ST&C

100% STRENGTHS

COLLAPSE	BURST	TENSION
4,010	4,790	132,000

DESIGN SAFETY FACTORS

COLLAPSE:	1.125
BURST:	1.0
TENSION:	1.8

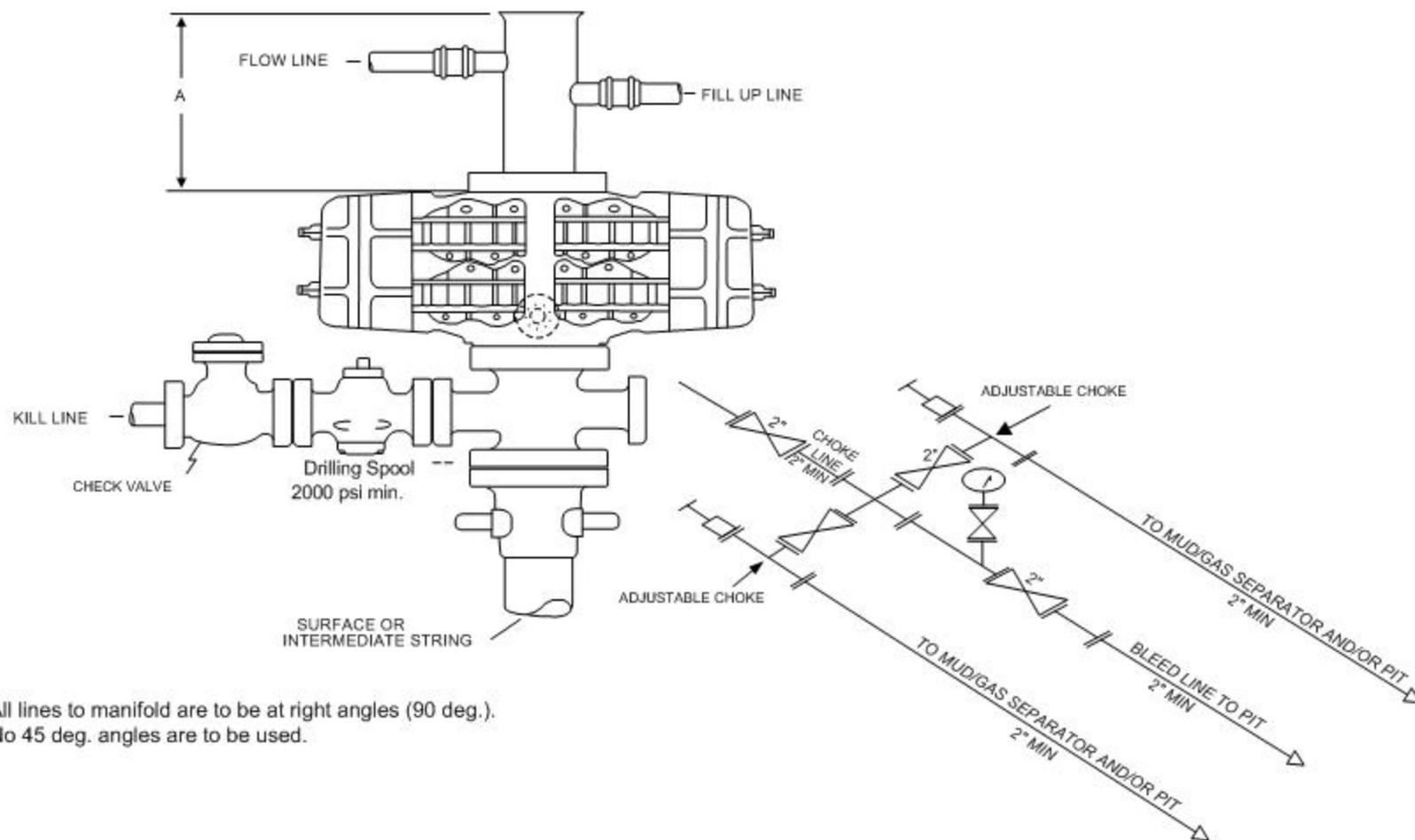
CALCULATED SAFETY FACTORS

COLLAPSE:	1.2	OK
BURST:	3.3	OK
TENSION:	1.9	OK

CALCULATED SAFETY FACTORS

Collapse:					
Hydrostatic Pressure:	0.052	9.5 ppg	6,760'	= 0.052 X 9.5 X 6,760' =	3339 psi
Safety Factor (Collapse):	4,010 psi	3,339 psi	1.2		OK
Safety Factor (Burst):	4,790 psi	1,440 psi	3.3		OK
Tension:	10.50 ppf	6,760'		= 10.5 X 6,760' =	70,980 lbs
Safety Factor (Tension):	132,000	70,980	1.9	= 132,000 / 70,980' =	OK

ANNULAR PREVENTER MAY BE SUBSTITUTED FOR DOUBLE GATE PREVENTERS



All lines to manifold are to be at right angles (90 deg.).
No 45 deg. angles are to be used.

2M CHOKES MANIFOLD EQUIPMENT – CONFIGURATION MAY VARY

BLOWOUT PREVENTER

2,000 psi minimum